

Short course on Frequency and amplitude stability in oscillators from RF/microwaves to optics

Course for PhD Students, Postdoc Fellows, and Young Scientists

Enrico Rubiola

FEMTO-ST Institute, Time and Frequency Department

<http://rubiola.org>

Spring 2013

1 General Information

This course derives from a series of seminars given at the *tutorial session* of international conferences of time and frequency, and also under invitation in a few prestigious laboratories (INRIM/Torino, University of Pisa, JPL/Pasadena, DESY/Hamburg, LBNL/Berkley, ANL/Chicago, MPI-QO/Munich...).

A choice has been made, fitting the material in the allocated time. More seminars are available, upon request. Best, addressing requests *also* to the Ecole Doctorale.

Lecture		Public		
no.	Title	Time & freq.	Physics & optics	Experim. Sciences
1	The measurement of power spectra			
1A	Basics and instruments			
1B	The cross-spectrum experimental method, with applications	■ ■ ■	■ ■ ■	■ ■ ■
2	Basic instruments and tools for the measurement of time and frequency [Req.1]			
2A	Phase noise and frequency stability	■ ■ ■	■ ■	■
2B	High-resolution time and frequency counters	■ ■ ■	■ ■	■
3	Phase noise and frequency stability in oscillators [Req. 1, 2]			
3A	The Leeson effect – the mechanism of oscillator instability and noise	■ ■ ■	■ ■	■
3B	The Pound Drever Hall frequency control	■ ■ ■	■ ■ ■	■ ■ ■

Audience. This course is intended as a *must* for all the Ph.D. students working on projects more or less related to time and frequency, including optics and astronomy. Other people may be interested, on the ground of the relevance of the domain.

The first lecture is of surprisingly broad interest. Then, “the appetite comes with eating,” says an old Latin proverb.

Young scientists, engineers, and guests are welcome.

Prerequisites. It is understood that the attendee background is suitable to a PhD thesis in experimental sciences or in engineering, and that he/she has a reasonable understanding of physics and electricity.

Language. All lectures are given in English, and all the learning material is written in English. However, the instructor understands well Italian and French.

2 Instructor

Enrico Rubiola is an internationally recognized scientist in the field of oscillators, frequency stability, and AM-PM noise from the low RF region to optics, and also precision instruments. Born in Italy in 1957, he has been a Researcher with the Politecnico di Torino, a Professor with the University of Parma, Italy, a Professor with the Université Henri Poincaré, Nancy. In 2005, he joined the Université de Franche Comté and the Femto-ST Institute, Besançon, and he lived in the USA in the meanwhile. He has investigated on various topics of electronics and metrology, like, navigation systems, time and frequency comparisons, atomic frequency standards, and gravity.

When the French *Programme d'Investissement d'Avenir* was launched in 2010, Enrico Rubiola took in charge the leadership of the local proposals related time and frequency. All the three proposals have been awarded (Oscillator IMP, First-TF, and Refimeve+). Prof. Rubiola has authored or co-authored about 150 articles in international journals, conferences and edited books, and has written three books. One more is in progress. He serves as a reviewer for a few journals of electrical engineering, physics and optics, and served as an associate editor for a IEEE journal. A wealth of articles, slides, and open literature is available on the home page <http://rubiola.org>.

3 Learning material

1. All the seminar slides will be distributed via the Enrico's home page <http://rubiola.org>.
2. Hundreds of copyright-free slides are available from <http://rubiola.org> (“seminar slides ≥ 1 H”), and several reports interests (“open literature”).
3. E. Rubiola, *Phase noise and frequency stability in oscillators*, Cambridge University Press 2008 (hardbound) and 2010 (paperback). A Chinese edition is scheduled for Summer 2013.
4. A few chapters (about 200 pages) of the forthcoming book *The measurement of AM and PM noise* will be available to the attendees.

4 Lecture 1 – The measurement of power spectra

4.1 Basics and instruments

Basics of spectral analysis. Inside the spectrum analyser and the FFT analyser. Measurement time, frequency resolution, spectral leakage, background noise, precision, accuracy, etc. Mathematics joins electronics and dirty tricks. In synthesis, it took me ten years to learn it from the experiments.

4.2 The cross-spectrum method

A physical quantity $c(t)$ is measured with two separate instruments, each of which adds its noise. Thus, the available signals are $x(t) = c(t) + a(t)$ and $y(t) = c(t) + b(t)$, where $a(t)$ and $b(t)$ are the instrument noise. All the signals are assumed to be stationary and ergodic, which means that the physical experiment is repeatable and reproducible. By correlating and averaging the two outputs $x(t)$ and $y(t)$, and assuming that the two instruments are independent, it is possible to extract the statistical properties of $c(t)$ and to reject the instrument noise. Thanks to the Wiener-Khinchin theorem, the average product of the Fourier transform of $x(t)$ and $y(t)$ converges to the power spectrum of $c(t)$.

The single-channel noise is rejected proportionally to the square root of the number m of averages, and ultimately to the square root of the measurement time. Of course, the two channels must be independent. The background noise is limited by the thermal inhomogeneity of the system instead of the absolute temperature. The observation of the cross-spectrum as a function of m enables the validation of the result in some weird cases, in which a low-noise reference is not available (AM noise, laser RIN, etc.).

A major improvement results from combining the correlation methods with other experimental methods, like the bridge measurement, the differential measurement, and the synchronous detection. Applying these ideas to phase noise measurements, a background noise of parts in 10^{-21} rad²/Hz (white) and of 10^{-18} rad²/Hz (flicker at 1 Hz) has been reported. The latter value, turned into a length fluctuation through the wavelength of the 9.2 GHz signal, is equivalent to 4.9×10^{-12} m. This is more than 10 times smaller than the Bohr radius of the electron.

4.3 Application examples

The cross-spectrum method is the basis of the correlation receiver used in radio-astronomy, with which R. Hanbury-Brown measured the first radio sources in the Cassiopeia and Cygnus constellations. The correlation radiometer followed, opening the way to the re-definition of the temperature in terms of fundamental constants. Batteries and of other dc references has been measured in this way, and of course the PM and AM noise of RF/microwave signals, microwave photonic signals, and laser RIN. In semiconductor technology small random signals reveal impurities, defects and energy traps of a dc-biased sample. Another exotic application is the measurement of electromigration in metals at

high current density, through the asymmetry between AM and PM $1/f$ noise, which impacts on VLSI technology.

5 Lecture 2 – Basic instruments and tools for the measurement of time and frequency

5.1 Phase noise and frequency stability

Random phase fluctuations, referred to as phase noise and closely related to frequency stability, affect precision and accuracy of timing. Random amplitude fluctuations, far less studied, may limit the most demanding experiment and systems. These types of noise impacts on numerous fields and applications, like metrology, physics, digital electronics, radars, telecommunications, optics, microwave photonics, gravitation measurements, particle accelerators, etc.

Phase noise is usually described in terms of one-sided power spectral density (PSD) $S_\varphi(f)$ of the random phase $\varphi(t)$. Other quantities often used and related to $S_\varphi(f)$ are the PSD of the fractional frequency fluctuation $y(t)$, denoted with $S_y(f)$, and the two-sample (Allan) variance $\sigma_y^2(\tau)$, as a function of the measurement time τ . The same apply to the fractional amplitude fluctuation $\alpha(t)$

Besides obvious thermal noise and shot noise, AM and PM noise rises from near-dc phenomena that modulate the system parameter. This describes flicker, and also fluctuations of the environment. The rules to propagate AM-PM noise through a system depend on the noise type, and may be surprising.

PM noise is often measured by converting $\varphi(t)$ into a voltage with a mixer. The measurement of oscillators requires a reference, either another oscillator or a discriminator. Ultimate sensitivity is achieved with the bridge (interferometric) method. After suppressing the carrier by adding an equal and opposite signal, the noise sidebands are amplified and converted to near-dc by synchronous detection.

Correlation and averaging helps rejecting the instrument noise when the signal is measured with two separate (statistically independent) instruments, each of which adds its noise. The sensitivity is limited by the thermal homogeneity, instead of the absolute temperature. This method is of special interest in the measurement of AM noise and laser RIN because even if the detector has sufficient sensitivity, we cannot validate the instrument without a reference low-noise source.

5.2 High-resolution time and frequency counters

Virtually all domains of physics and engineering at some point rely on time-and-frequency metrology, and in turn need high resolution counters.

The early instruments are based on the direct counting of the integer number of pulses in a reference time interval. This is referred to as coarse counting. The resolution associated to counting an integer number of pulses is of one cycle of the clock frequency. Ultimately, the resolution is limited by the maximum toggling frequency of the digital technology. For example, with a 100 MHz

clock it is possible to measure a time interval with a resolution of 10 ns, hence a frequency with a resolution of 10^7 at 100 ms, etc. As of 2012, small FPGAs can toggle at 1 GHz clock. Higher resolution is obtained by interpolating the clock edges.

The simplest interpolator is the multi-tap delay line. Implementation in a gate array is amazingly simple, based on the fact that the internal delay of the single gates is small and predictable. A resolution up to 100 ps is expected. Other interpolators are found in the literature, namely, the analog integrator, the frequency vernier, and the dispersive SAW filter. Commercial counters based on these methods achieve a resolution of 1–100 ps. For reference, in a coaxial cable the light travels 200–250 μm in 1 ps. Albeit the design can be tricky, the principles are simple to understand.

A trivial way to measure a frequency is to count the number of cycles — a fractional number in the case of interpolating counters — over a reference time τ defined by start and stop events. At a closer look, the readout is the frequency $\nu(t)$ averaged over τ with uniform weight. A frequency counter working in this way is called Π counter. This term derives from the graphical similarity of the Greek letter Π with the rectangular (uniform) weight function. The Π counter suffers from white noise, chiefly the trigger noise. For example, a jitter of 10 ps rms at both start and stop yields a fractional-frequency resolution of 1.41×10^{-10} in $\tau = 100$ ms.

Improved resolution is obtained by averaging on highly overlapped measurements, which is equivalent to averaging the frequency $\nu(t)$ triangular weight, and for this reason the instrument is called Λ counter. Notice that the triangular weight spans on a time 2τ instead of τ . This type of measurement is equivalent to linear regression of the input frequency, based on a series of uniformly-spaced time stamps. Averaging on m overlapped measures, the resolution improves by \sqrt{m} . In the above example, averaging on $m = 10^4$ measures yields a resolution of 1.41×10^{-12} .

The Π counter is naturally suitable to the direct evaluation of the Allan variance. By contrast, feeding a stream of data measured with a Λ counter in the formula of the Allan variance, gives the modified Allan variance if the triangles are overlapped by τ , and something else if the triangles are overlapped otherwise, or if there is a dead time. Given a stream of measurement taken over τ , decimation enables to get new data streams averaged on 2τ , 4τ , 8τ , etc. Decimation turns out to be tricky, and interpretation mistakes are around the corner if the instrument internal mechanisms are well understood and under full control.

6 Lecture 3 – Oscillator and laser stability

6.1 The Leeson effect — The mechanism of instability and noise

Simply stated, an oscillator is of a loop in which a resonator sets the oscillation frequency and an amplifier compensates for the resonator loss. The oscillation amplitude is set by gain saturation, usually in the amplifier. When phase noise

is introduced in the loop, the oscillator converts it to frequency noise through a process of time-domain integration. The consequence is that the oscillator phase fluctuation diverges in the long run. This phenomenon was originally referred as the “Leeson model” after a short article published by D. B. Leeson. On my side, I prefer the term “Leeson effect” in order to emphasize that it is far more general than a simple model.

The first part of this tutorial explains the phase-to-frequency conversion mechanism as a general phenomenon inherent in the feedback, following an heuristic approach based on physical insight. There follow the relationships between the noise of the internal components (sustaining amplifier, resonator, etc.) and the phase noise at the oscillator output, or equivalently the frequency stability.

The second part is the analysis of the phase noise spectra found in the data-sheet of commercial oscillators: dielectric-resonator oscillator (DRO), whispering gallery oscillator (WGO), 5–100 MHz quartz crystal oscillators, optoelectronic oscillator (OEO). The analysis gives information on the most relevant design parameters, like the quality factor Q and the driving power of the resonator, and the flicker noise of the sustaining amplifier.

The last part shows the derivation of the oscillator phase noise formulae from the elementary properties of the resonator. Interestingly, the amplitude non-linearity, necessary for the oscillation amplitude to be stable, splits the resonator relaxation time into two time constants. The approach shown in this last part is general. It applies to all oscillators, including quartz, RLC, microwave cavity, delay-line, laser, etc.

6.2 The Pound Drever Hall frequency control

The PDH frequency control is a milestone in radio engineering and in spectroscopy, and a smart and powerful tool available to numerous branches of experimental science.

First published in 1946 by Robert Pound, a member of the Radiation Laboratory golden team, the ‘Pound control’ was ported to optics by John Hall (Nobel prize in 2005) and R. Drever. The PDH control is nowadays the standard method to control a microwave oscillator or a laser oscillators to an external frequency reference, like a dielectric resonator or a Fabry-Pérot cavity.

The unique feature of the PDH scheme, which makes it superior to all competitors, is that the path length from the locked oscillator to the reference resonator cancels, so its fluctuations. Furthermore, locking relies on a null measurement of the frequency error.

Most used in general microwave and optics, this technique is the one and only which can be used at $10^{-15} \dots 10^{-16}$ frequency stability level (Femto-ST ULISS oscillator, and photonic oscillators). Applications span in a wide range: metrology, optics, spectroscopy, gravitation, space/military electronics, etc.